## Appendix 3.33 Estimated Odour Emission Reduction by Improvement of DWFI Inerception Efficiency Derivation of BOD loading in New Yau Ma Tei Typhoon Shelter

Table 1 Deduction of BOD loading in the New Yau Ma Tei Typhoon Shelter

Column ID		(a)					(b)		(c)		(0	i)	(e)	(f)	(g)	(h)	(i)	(0)	(p)	(q)	(r)
	Reference				Outflow (n	n³/d)									Phase I	Pollution Loadi	ng Survey ·	Water Qual	ity Sampling Resul	ts	
Location		DWFI number	Current invert height (mPD)	T s t E Inflow (m³/d) S	o tormwater To Drainage Se System sys	) I ewerage I stem (	Percentage Interception (%)	BOD loading from sampling event (kg/d)	Theoretical BOD Loading from Drainage Catchment (kg/d)	Tidal influence?		TBOD <sub>tot</sub> , Theoretical BOD Loading from drainage catchment x tidal loading percentage of influence (25% for tidal influence, 12% for no tidal influence, Tables 4.26 and 4.27)	TBOD = TBODtot *(yi)	ID	Flow (m³/d)	TSS (kg/d) C	COD (kg/d)	NH3-N (kg/d)	BOD₅ Loading from sampling event	Percentage of Pollution Loading	γi Relative percentage of pollution loading in Drainage catchment according to Table 4.25
Reference		Figure 4.17	Figure 8.24 78.30		Table 4	l.31		Ta	ble 4.25	Table 4.30	For DWFI 2, 3 & 4. Based on tide information and invert levels Figures 8.24-8.30	Table 4.25, 4.26, 4.27		Figure 4. Table 4.2	15 22 - samples coll	ected at the ou (4.7.42)	utlet of the	box culverts	Tat	ole 4.23	
Lai Chi Kok Park BC				10.105	7.540	A SEE	20.00/	1,068	19,570			2,348	3	L10	56,841	1,783	3,613	19	1,06	8 3.39	0
Hinn Wah Street BC		14		12,195	7,540	4,000	30.2%	3 100	6 346			763	<b>b</b>	113	31,593	637 972	3,340	210	1,51	0 4.77 1 199	0
Fat Chueng Street BC		13	8					//////////////////////////////////////	//////////////////////////////////////		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	<u></u>	***************************************	L14	1,244	18	141	5	5 3	5 0.1%	6
	<b> </b>	10	)	1						Y				L16	87,409	1,057	8,875	78	3 1,869	9 5.8%	6
Tonkin Street BC								2,761	11,687		Y	2,922	2	L17	44,468	401	4,549	43	8 85	7 2.7%	6
		8	8							Y				L19	38,286	605	2,911	119	792	2 2.5%	6
Nam Choong Street BC														L20	37,463	561	4,155	108	3 /2	2 2.3%	6 / -
Wai On Street BC	+			+				3.092	15.822		Y	3.955	5	L22	15.094	1.641	1.355	150	474	4 1.5%	0
Tai Kok Tsui Road		7	,					0,001	10,022				5	L35	23,901	2,710	6,685	297	3,11	5 9.7%	6 27.09
Nullah Road BC		6A		566,070	561,000	5,070	0.9%			Y			1,98	5 L24	60,399	2,036	5,878	344	2,45	1 7.7%	6 21.2%
Nelson Road BC		e	5	8,199	4,215	3,984	48.6%						1,36	3 L25	30,599	2,252	3,897	163	1,68	3 5.3%	6 14.6%
Shantung Street BC													1,46	1 L26	16,350	1,888	2,882	117	7 1,804	4 5.6%	6 15.6%
Soy Street BC		5	5	22,122	15,730	6,392	28.9%	11,555	37,424		Y	9,356	6 2,02	6 L27	25,872	2,996	5,692	177	2,502	2 7.8%	6 21.79
		4	+1.57	7			32.4%						26	4 L28	13,106	649	1,692	73	45	0 1.4%	4.39
Dundas Street BC	alis sa uta al ta					<mark>L</mark>							62	9 129	22,719	547	2,875	150	1,07	o 3.4%	6 10.3%
Waterlee Read BC	diverted to	3	5										36	5 L30 G L31	15,406	541 661	2,007	165	62	9 2.0% 1 3.0%	6.0%
Public Square Street BC			+12				32 /%						1.46	5 L 32	21 370	919	2,450	216	2 50	3 7.8%	24.09
Saigon Street BC			+1.2	-			52.476						2 21	2 1.33	32 031	1 426	6 848	323	3 77	S 11.8%	36.29
				+									56	6 L34.1	17,072	408	1,971	119	96	7 3.0%	9.39
Jordon Road BC								10,428	24,425		Y	6,106	6 3	2 L34.2	1,629	21	125	18	5	5 0.2%	<mark>6</mark> 0.5%
													-						32,004	4 100%	6
NOTES							No efficiency information available - Assume average of all other DWFIs				No information available on tidal influence - Assume tidal influence due to invert levels shown in Figure 8.24 - 8.30 and tide information		=percent of pollution loading / (sum percent of pollution loading for BC [column (r)] * (Theoretical BOD loadin from drainage catchme x tidal loading percentage of influence [column (d)]	of ) ng ))							= Percentage o Pollution Loading [colum (q)] / sum Percentage of Pollution Loading [colum (q)]
Conservative interception efficiency based on published information (max interception efficiency = 85.5% as for DWFI No. 14 below, and Feasibilty Study, Section 8.2, interception efficiency = 88%) Lai King Hill Road/Kau Wah Keng Yuen Chow Street Kwong Lee Street Cheung Shun Street Kom Tsun Street/Cheung Sha Road	Figure 3.6 Figure 3.6 Figure 3.6 Figure 3.7 Figure 3.6	KT 9 - YC9 to YC1 11 14		3422 3487 1740	3032 504 1410	390 2983 330	80.0% 11.4% 85.5% 19.0%			Y											

Notes: Review of West Kowloon and Tsuen Wan Sewerage Master Plans - Feasibiliy Study (Feb 2010)

Table 4.22 - Daily Pollution Loads in Stormwater Drainage SystemTable 4.23 - Distribution of Pollution Loading in West KowloonTable 4.25 - Percentage of DWF Discharge at Box Culverts by Drainage CatchmentTable 4.26 - Percentage of DWF Discharge to Tsuen Wan Coast (Including Mixing Zone Concentration)Table 4.27 - Percentage of DWF Discharge to Tsuen Wan Coast (Excluding Mixing Zone Concentration)Table 4.30 - DWFI Monitoring ResultsTable 4.31 - Assessment of Average Daily Dry Weather Flow Interception

## Table 2 Tide information

Historic Tide Mid-Level

+1.3 mPD

I					
				Mean	Mean Lower
				Higher High	Low Water
				Water Level	Level
	Location	Period of Data	Mean	(mPD)	(mPD)
ſ	Quarry Bay/North Point	1981-1999	1.3	2	0.5

Notes: Reference made to: PORT WORKS DESIGN MANUAL - Part 1 General Design Considerations for Marine Works Civil Engineering Office Civil Engineering Department The Government of the Hong Kong Special Administrative Region

## Table 3 DWFI efficiencies

DWFI	Measured Interception Efficiency	Theoretical BOD loading before DWFI leading to NYMTTS	<sup>T</sup> BOD <sub>M</sub> Theoretical BOD loading entering NYMTTS at measured interception efficiency	TBOD <sub>R</sub> Theoretical BOD loading entering NYMTTS at the assumed highest interception efficiency of 80.0% (note a and b)	% Overall reduction of BOD loading entering NYMTTS ( <sup>T</sup> BOD <sub>M</sub> - <sup>T</sup> BOD <sub>R</sub> ) / <sup>T</sup> BOD <sub>N</sub>	
6A 6 5	0.9% 48.6% 28.9%	1985 2823 2026	1967 1451 1440	393 290 288	00.00/	Cherry St
3 & 4 2 no DWFI	32.4% 32.4% 0.0%	6834 1830 3678 598 6106	4859 1237 2487 598 4323	972 366 736 598 1700	<u>80.0%</u> 60.7%	BC Jordon Rd BC
Notes		0100	4323	1700	60.7%	BC

For Cherry St a new DWFI is to be installed at the NYMTTS (see Appendix 3.36). This is assumed to have an interception efficiency of 80.0%. This mean for Cherry St BC, the stormwater goes through 1 set of DWFI and then a second DWFI at 80% efficiency. The overall reduction of water entering the NYMTTS at Cherry St compared to the current situation is 80%

For Jordan Road, the interception efficiency of the existing DWFI are to be improved (see Appendix 3.36) to an assumed interception efficiency of 80%. This means the current DWFI interception will improve from 32.4% to 80.0%. This results in a reduction of 60.7% of stormwater entering NYMTTS when compared to the current situation

(b)

(a)

Table 4 Contribution of water to NYMTTS odour	
Table 4 Contribution of water to NTMTTO Guodi	

Grid number	Date	Background ambient odour (ou/m <sup>3</sup> )	Odour from Air (total), at water surface (ou/m <sup>3</sup> ) (A)	Odour from Water (ou/m³) (B)	Odour from Sediment (ou/m³)	Odour contribution from water
						= (B) / (A)
30	18-Feb	229	2632	1334	299	51%
	20-Feb	240	2168	2118	463	98%
7	18-Feb	98	1722	1051	10	61%
	20-Feb	389	3373	2723	10	81%
					average	0.728

Note Information obtained from onsite sampling, more details can be found in Appendix 3.26b